

An Efficient Approximation of Optimal Damping in Mechanical Systems

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[WORKSHOP ON CONTROL OF DYNAMICAL SYSTEMS,

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The talk contains results from

N. Truhar, and I. Nakić; *Damping Optimization Of Mechanical Systems;* work in progress

M. Petrač, N. Truhar and I. Nakić; *Damping optimization of linear* vibrational systems with a singular mass matrix; submitted



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$$\begin{aligned} M\ddot{x} + D\dot{x} + Kx &= 0, \\ x(0) &= x_0, \quad and \quad \dot{x}(0) &= \dot{x}_0 \end{aligned}$$

where $M, D, K \in \mathbb{R}^{n \times n}$ (mass, damping, stiffness), M and K > 0 (positive definite).

 $D=C_u+C,\,C_u>0 \text{ internal damping},\,C\geq 0 \text{ external (viscous)} \\ \text{damping}.$



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A very important question arises in consideration of such systems:

For the given mass (M) and stiffness (K) determine the best (optimal) damping which will insure an optimal evanescence.



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 $D=C_u+C, \, C_u>0 \text{ internal damping, } C\geq 0 \text{ external (viscous)} \label{eq:constraint}$ damping.



Consider *n-mass oscillator or oscillator ladder*



 $m_i > 0$ - masses, v_i - viscosity applied on the i-th mass, $k_i > 0$ - stiffnesses



Consider n-mass oscillator or oscillator ladder m_{\perp} m_2 m_3 m_n $\bigvee_{k_1} \underbrace{v}_{k_2} \underbrace{k_3}_{k_3} \underbrace{v}_{v} \underbrace{w}_{v} \underbrace{w}$

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Consider *n*-mass oscillator or oscillator ladder $M = \text{diag}(m_1, m_2, \dots, m_n), \quad D \equiv C_u + C = C_u + v_1 e_1 e_1^T + v_3 e_3 e_3^T.$ $K = \begin{pmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 + k_3 & -k_3 \\ & \ddots & \ddots & \ddots \\ & & -k_{n-1} & k_{n-1} + k_n & -k_n \\ & & & -k_n & k_n + k_{n+1} \end{pmatrix}$

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For this optimization problem one needs optimization criteria

• Spectral abscissa criterion

 $\max_{k} \operatorname{Re}\left(\lambda_{k}\right) \quad \to \quad \min$

where λ_k are the complex eigenvalues of $\left(\lambda^2 M + \lambda D + K
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• we will use the following criterion:

 $\operatorname{tr} X \to \min$

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For the moment we assume: given dampers' positions ! We optimize dampers viscosities v_1, \ldots, v_r

$$A(v)X(v) + X(v)A(v)^{T} = -Z$$
 $v = (v_{1}, ..., v_{r})$

Z depends on dominant frequencies.

Standard approach:

- Pick (define) dampers position
- Solve Lyapunov equation (Bartels-Stewart or Hammerling (Schur) algorithm)
- using obtained orthogonal basis to calculate Gradient and Hessian
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All direct methods for trace calculate whole solution - to expensive. For Example:

n = 600, r = 2, 2 similar dampers, fixed positions

with a proper starting point v_0 ; viscosity optimization

Hammarling algorithm $\sim 3\cdot 10^{12}~~{\rm flops}=3~~{\rm teraflops}.$ $\sim 20~{\rm min}~{\rm (2~GHz,~2~GB)}$

Positions' optimization:



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We have notices:

- "Bad positions" can not be significantly improved by viscosities
- For detecting "bad positions" (better a good), we do not need 16 or even 8 exact digits.
- \diamond We will try to find a small number of "good positions".

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Idea:


Let $\Phi^T K \Phi = \Omega^2$, $\Phi^T M \Phi = I$, for i = 1, ..., n, compute minimal traces $tr_{opt} = tr(X_k(i))$, where

 $A(i)X_k(i) + X_k(i)A(i)^T = Z_k, Z_k = \widehat{Z}_k \oplus \widehat{Z}_k, (\widehat{Z}_k)_{jk} = \delta_{j,k},$

 $k=1,\ldots,s.$

$$A(i) = A_0 - v_i \begin{bmatrix} 0 & 0 \\ 0 & c_i c_i^T \end{bmatrix}, A_0 = \begin{bmatrix} 0 & \Omega \\ -\Omega & -\alpha \Omega \end{bmatrix}, \quad c_i = \Phi^T e_i,$$

 $i=1,\ldots,n$. For each $k=1,\ldots,s$ we get function $g_k:\{1,\ldots,n\} o \mathbb{R}$

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The possible best positions are local minimums of $g_k(i)$ for i = 1, ..., n.



Consider system on figure, n = 601





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Left figure is for the 5-th frequency (s = 5).

Right figure is for the 8-th frequency (s = 8). The candidate: 339(0.3688), 415(0.4285), 487(0.4324), 561(0.3698) (for s = 5) The candidate: 326(0.3618), 375(0.4180), 425(0.4326), 477(0.4333)

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For $s=1,\ldots,40$ instead 180000~(n=601) possibilities, we get $9000~(n_0=176)!$

Still, it is very demanding job! 9000 2D optimizations.

We need: a efficient solver (faster then n^2) and more efficient optimization Case without internal damping: $C_u = 0$, there exist formula: Veselić (1990):

$$Tr(ZX) = const + \frac{a}{v} + bv, \quad a, b > 0.$$

total cost $\mathcal{O}(n^2)$, optimal v for free, $v_{opt} = \sqrt{a/b}$. Unfortunately, for $C_u \neq 0$, the above formula is very unstable. Idea: derive a similar formula (even complicated) for $C_u \neq 0$!

We failed! It still open?



For s = 1, ..., 40 instead 180000 (n = 601) possibilities, we get 9000 ($n_0 = 176$)! Still, it is very demanding job! 9000 2D optimizations. We need: a efficient solver (faster then n^2) and more efficient optimization Case without internal damping: $C_u = 0$, there exist formula: Veselić (1990):

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We failed! It still open?



For $s=1,\ldots,40$ instead 180000~(n=601) possibilities, we get $9000~(n_0=176)!$

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Now we can apply the optimization process (similar as parabolic minimization):

define rational functions

$$g(v) = \frac{av^2 + bv + c \cdot \operatorname{tr}(X(0))}{v + c},$$

a, b and c are determined by a simple interpolation through v_1, v_2, v_3 . The zero of $g'(v_4) = 0$ is the first approximation for the optimal v. Replace $\{v_1, v_2, v_3\}$ by the new minimum v_4 and repeat the process until the selected tolerance level is attained.

We noticed: that 5-10 steps are enough for tolerance $pprox 10^{-4}.$

Still we need to solve 5-10 Lyapunov equations, with a low tolerance ($\approx 10^{-4}$).



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For efficient optimization, we need an apriority error bound.

Unfortunately, up to date we did not find usefull apriority error bound (for any existing "fast solvers")

Thus, we derive a new error bound.

Let

$$A^T X + X A = -Z,$$

be the Lyapunov equation, with

$$A = \begin{bmatrix} 0 & A_{12} \\ -A_{12} & -\Delta \end{bmatrix}, \quad Z = \begin{bmatrix} Z_1 & 0 \\ 0 & Z_2 \end{bmatrix},$$

with A_{12} and $\Delta > 0$.

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Let $E \doteq A^T Y + YA + Z$, be residual, written

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If A_{12} is diagonal, then the following (new) bound holds

 $|\operatorname{tr}(X-Y)| \lesssim |\operatorname{tr}(\Delta^{-1}E_3)| + |\operatorname{tr}(E_2A_{12}^{-1})| \doteq Bnd.$



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For illustration let r = 2, i.e. number of positions is 2 **Input:**

 \varOmega – undamped frequencies

(square root of eigenvalues of the pair M and K);

s – the number of dominant undamped frequencies (2s = rankZ);

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form a set of quadruples (possible minimums) $(s_1(t), s_2(t), v_1(t), v_2(t)), t = 1, \ldots T_0 \cdot (T_0 - 1)/2$, usually (for r = 2) $T_0 \le 0.3n$. **Phase II:**

for each quadruple $(s_1(t), s_2(t), v_1(t), v_2(t))$ calculate corresponding trace of the solution of Lyapunov equation

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$$A_p(s,v) = A_0 - v_1(t) \cdot c_{s_1(t)} c_{s_1(t)}^T - v_2(t) \cdot c_{s_2(t)} c_{s_2(t)}^T,$$

$$(s_{\min}, v_{\min}) \doteq (s_1, s_2, v_1, v_2)_{\min} = \operatorname*{argmin}_{1 \le t \le \widehat{T}_0} \operatorname{tr}(Y(t)).$$



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For n = 50Our approach: 33 potential positions, ($n \times 1D$ opt. +528 Lyap. sol.) \Rightarrow opt. pos. (16, 31); opt. visc. (18.5, 25.4). after 13 sec. opt. trace 651.82



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For n = 100Our approach: 59 potential positions, ($n \times 1D$ opt. +1770 Lyap. sol.) \Rightarrow opt. pos. (14, 98); opt. visc. (30.5631, 35.7604). after 157 sec. opt. trace 1428.2



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Case II n = 1000 $m_i = 100(i - 1) + 2, k_i = 1, i = 1, \dots, n,$ $Z = I_{100} \oplus 0_{900}, \oplus I_{100} \oplus 0_{900}, M = \text{diag}(m_i)/(\sum m_i).$ Our approach: 45 potential positions (with 292 different viscosities), $(n \times 1D \text{ opt.} + 42486 \text{ Lyap. sol.}) \Rightarrow \text{opt. pos.} (292, 830); \text{opt. visc.}$ (0.0469, 0.0744).Using projection with p = 200, we need approx. 2.5 hours vs. standard approach 1000 potential positions, $(499500 \times 2D \text{ opt. each} \approx 40 \times \text{ Lyap. sol.});$ No Way !!! approx. 5550 hours





Figure: n mass oscillator

${\rm Case ~II}~n=1000$

$$\begin{split} m_i &= 100(i-1) + 2, k_i = 1, i = 1, \dots, n, \\ Z &= I_{100} \oplus 0_{900}, \ \oplus I_{100} \oplus 0_{900}, \ M = \mathrm{diag}(m_i) / (\sum m_i). \\ \text{Our approach: 45 potential positions (with 292 different viscosities) , } (n \times 1D \text{ opt.} + 42486 \text{ Lyap. sol.}) \Rightarrow \text{ opt. pos.} (292, 830); \text{ opt. visc.} \\ (0.0469, 0.0744). \\ \text{Using projection with } p = 200, \text{ we need approx. 2.5 hours} \\ \text{vs. standard approach 1000 potential positions, } (499500 \times 2D \text{ opt. each} \\ \approx 40 \times \text{ Lyap. sol.}); \text{ No Way !!! approx. 5550 hours} \end{split}$$





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We still consider a system:

$$M\ddot{x} + C\dot{x} + Kx = 0$$
, $x(0) = x_0$, $\dot{x}(0) = \dot{x}_0$,

where $M \ge 0, C \ge 0$ and K > 0. Simult. diagonal.

$$\Phi^T M \Phi = \begin{bmatrix} 0_{n_0} & \\ & I_m \end{bmatrix}, \qquad \Phi^T K \Phi = \begin{bmatrix} \Omega_0^2 & \\ & \Omega_+^2 \end{bmatrix},$$



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Now, the damping

$$D = \Phi^T (C_{in} + v \cdot C_{ex}) \Phi = \begin{bmatrix} D_{11} & D_{12} \\ D_{12}^T & D_{22} \end{bmatrix},$$
$$D_{11} \in \mathbb{R}^{n_0, n_0}, \quad D_{22} \neq 0.$$

All this implies

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which yields to the following linearization:

$$\dot{z} = Az,$$

$$A = \begin{bmatrix} -\Omega_0 D_{11}^{-1} \Omega_0 & 0_{n_0,m} & -\Omega_+ D_{11}^{-1} D_{12} \\ 0_{m,n_0} & 0_{m,m} & \Omega_+ \\ D_{12}^T D_{11}^{-1} \Omega_+ & -\Omega_+ & D_{12}^T D_{11}^{-1} D_{12} - D_{22} \end{bmatrix}$$

If $D_{12} = 0$, then the linearization

$$A_{+} = \begin{bmatrix} 0 & \Omega_{+} \\ -\Omega_{+} & -D_{22} \end{bmatrix}$$

The standard linearization used I. Nakić 2002, K. Brabender 1998, Müeller and Gürgöze 1991, Benner, Tomljanović Truhar 2010, 2011.



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The standard linearization used I. Nakić 2002, K. Brabender 1998, Müeller and Gürgöze 1991, Benner, Tomljanović Truhar 2010, 2011.



The ODE system

$$\begin{split} \dot{z}_1 &= -\Omega_0 D_{11}^{-1} D_{12} z_3 - \Omega_0 D_{11}^{-1} \Omega_0 z_1 \\ \dot{z}_2 &= \Omega_+ z_3 \\ \dot{z}_3 &= D_{12}^T D_{11}^{-1} \Omega_0 z_1 - \Omega_+ z_2 + \left(D_{12}^T D_{22}^{-1} D_{12} - D_{22} \right) z_3 \,, \end{split}$$

which yields to the following linearization:

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Singular mass matrix – damping optimization



Here usually, $C_{in} = 0$ ($\alpha = 0$ or $\alpha \ll 1$). We optimize only v in $D_{ex} \doteq v \Phi^T C_{ex} \Phi$ $\operatorname{tr}(ZX) = \min$

For the $n_0 \doteq \dim(\mathcal{N}(M)) = 1$ and $\alpha = 0$ (no internal damping) we have

$$f(v) = \operatorname{tr}(X) = 2 \cdot \sum_{i}^{n-1} (X_{11})_{ii} + \sum_{i}^{n-1} \frac{\omega_n}{d_2} \frac{\eta_i}{\omega_i} (d_1)_i + v \frac{d_2^2}{2\omega_n^2} (2n-1).$$

Thus, we approximate the trace function with

$$f(v) = \frac{a_0}{v} + b_0 v + c_0,$$

where the constants a_0 , b_0 and c_0 are obtained from $tr(X)(v_i)$, i = 1, 2, 3.

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the novel approach for damping optimization for mechanical systems

It is based on the new:

position search, base on one frequency damping optimization viscosity optimization using new approximation for the trace function error bound for the approximate solution of Lyapunov equation

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formula for the trace of solution of Lyapunov equation 1D case

approximation function for the trace for 2D or 3D case



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