# Damping optimization in mechanical systems using parametric model reduction



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# Problem formulation Overview of optimization criteria



#### We consider vibrational system

$$M\ddot{q}(t) + \overbrace{(C_{int} + B_2 G B_2^T)}^{C(g) = \text{damping part}} \dot{q}(t) + Kq(t) = E_2 w(t),$$
 
$$y(t) = H_1 q(t).$$

- $M,K\in\mathbb{R}^{n\times n}$  mass and stiffness, the symmetric and positive definite
- $q \in \mathbb{R}^n$  state vector and y is output vector determined by  $H_1 \in \mathbb{R}^{\ell \times n}$ ,
- $E_2 \in \mathbb{R}^{n \times m}$  determines primary excitation matrix and vector  $w \in \mathbb{R}^m$  corresponds to primary excitation input.
- $C_{int} \in \mathbb{R}^{n \times n}$  internal damping e.g.  $C_{int} = \alpha_c C_{crit}$ , where

$$C_{crit} = 2M^{1/2}\sqrt{M^{-1/2}KM^{-1/2}}M^{1/2},$$

•  $G = \operatorname{diag}(g_1, g_2, \dots, g_k), g_i \geq 0$  damping coefficients.



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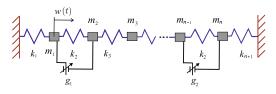
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#### Example: n-mass oscillator or oscillator ladder



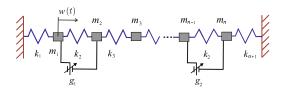
$$M = \operatorname{diag}(m_1, m_2, \dots, m_n), \quad C(g) = \alpha_c C_{crit} + B_2 G B_2^T,$$
  

$$B_2 G B_2^T = g_1 (e_i - e_{i+1}) (e_i - e_{i+1})^T + g_2 (e_j - e_{j+1}) (e_j - e_{j+1})^T.$$

$$K = \begin{pmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 + k_3 & -k_3 \\ & \ddots & \ddots & \ddots \\ & -k_{n-1} & k_{n-1} + k_n & -k_n \\ & & -k_n & k_n + k_{n+1} \end{pmatrix}$$



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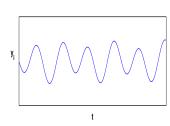
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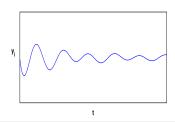


The principal goal is to determine an optimal damping matrix that will minimize the influence of the input w (viewed as a disturbance) on the output, y.





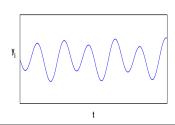
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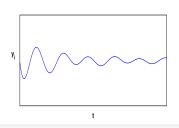


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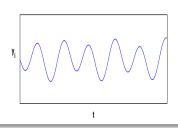
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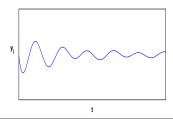


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# (M, K, D)





#### Linearization

With the substitutions  $x_1(t):=q(t), x_2(t):=\dot{q}(t)$  and  $x:=\begin{bmatrix}x_1\\x_2\end{bmatrix}$  we obtain a first-order representation of the closed-loop system

$$\underbrace{\begin{bmatrix} I_n & 0 \\ 0 & M \end{bmatrix}}_{\mathcal{E}} \dot{x}(t) = \underbrace{\begin{bmatrix} 0 & I_n \\ -K & -C(g) \end{bmatrix}}_{\mathcal{E}} x(t) + \underbrace{\begin{bmatrix} 0 \\ E_2 \end{bmatrix}}_{\mathcal{E}} w(t),$$

$$y(t) = \underbrace{\begin{bmatrix} H_1 & 0 \end{bmatrix}}_{\mathcal{E}} x(t).$$

Using the Laplace transform we obtain the closed-loop transfer function

$$\mathbf{H}(g,s) = H_1 \left( s^2 M + sC(g) + K \right)^{-1} E_2$$

$$= \begin{bmatrix} H_1 & 0 \end{bmatrix} \left( s \begin{bmatrix} I_n & 0 \\ 0 & M \end{bmatrix} - \begin{bmatrix} 0 & I_n \\ -K & -C(g) \end{bmatrix} \right)^{-1} \begin{bmatrix} 0 \\ E_2 \end{bmatrix}$$



# $\mathcal{H}_2$ norm of a system

#### Define the space

$$\begin{split} \mathcal{H}_2^{\ell \times m} := & \left\{ \mathbf{H} : \mathbb{C}^+ \to \mathbb{C}^{\ell \times m} \;\middle|\; \mathbf{H} \text{ is analytic in } \mathbb{C}^+ \text{ and} \right. \\ & \left. \int_{-\infty}^{+\infty} \operatorname{tr} \left( \mathbf{H} (\mathrm{i} \omega)^* \mathbf{H} (\mathrm{i} \omega) \right) d\omega < \infty \right\}, \end{split}$$

$$\|\mathbf{H}(g,\cdot)\|_{\mathcal{H}_2} = \left(\frac{1}{2\pi} \int_{-\infty}^{+\infty} \operatorname{tr}\left(\mathbf{H}(g,i\omega)^* \mathbf{H}(g,i\omega)\right) d\omega\right)^{\frac{1}{2}}.$$

It can be expressed via the solution of a Lyapunov equation, i.e.

$$\|\mathbf{H}(g,\cdot)\|_{\mathcal{H}_2} = \left(\frac{1}{2\pi}\operatorname{tr} B^T \mathcal{P} B\right)^{\frac{1}{2}}, \quad \text{where} \quad A^T \mathcal{P} + \mathcal{P} A = -C^T C$$

[T./Beattie/Gugercin18, Benner/Kurschner/T./Truhar16]



 $\mathcal{H}_{\infty}$  norm of a system <sup>1</sup> Define the space

$$\mathcal{H}_{\infty}^{\ell \times m} := \left\{ \mathbf{H} : \mathbb{C}^{+} \to \mathbb{C}^{\ell \times m} \;\middle|\; \mathbf{H} \text{ is analytic in } \mathbb{C}^{+} \text{ and } \sup_{s \in \mathbb{C}^{+}} \left\| \mathbf{H}(s) \right\|_{2} < \infty \right\}$$

$$\|\mathbf{H}(g,\cdot)\|_{\mathcal{H}_{\infty}} := \sup_{\lambda \in \mathbb{C}^+} \|\mathbf{H}(g,\lambda)\|_2 = \sup_{\omega \in \mathbb{R}} \|\mathbf{H}(g,i\omega)\|_2.$$

One can also consider certain mixed performance measures

- $\|\mathbf{H}(g,\cdot)\|_{\mathcal{H}_{\infty}/\mathcal{H}_{2}}$
- criterion that combines  $\|\mathbf{H}(g,\cdot)\|_{\mathcal{H}_2}$  and total average energy <sup>2</sup>

<sup>&</sup>lt;sup>1</sup>[T./Voigt20]



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<sup>&</sup>lt;sup>2</sup>[Nakić/T./Truhar19]



#### Main drawback of direct methods

#### Damping optimization (position and viscosity optimization):

In the n-mass oscillator:

$$C_{ext} = g(e_i - e_{i+1})(e_i - e_{i+1})^T + g(e_j - e_{j+1})(e_j - e_{j+1})^T,$$

there is a problem with determining optimal (i,j),  $1 \leq i \leq j \leq n$  and g.

For example if n=1000

discrete optimization over 500 000 different damping positions.

Efficient overall algorithm for optimization of damping positions is still needed!

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#### Consider a parametric LTI dynamical systems represented as

$$E\dot{x}(t;p) = A(p)x(t;p) + Bu(t),$$
  
$$y(t;p) = Cx(t;p),$$

where  $E, A(p) \in \mathbb{R}^{n \times n}$ ,  $B \in \mathbb{R}^{n \times m}$  and  $C \in \mathbb{R}^{l \times n}$ .

- $x(t;p) \in \mathbb{R}^n$  denotes the state variable
- $u(t) \in \mathbb{R}^m$  and  $y(t;p) \in \mathbb{R}^l$  represent the inputs and outputs of the system, resp.

We will denote this system with [E, A(p), B, C].



For parameter p we can approximate our system with reduced system  $\,^{1}$ 

$$E_r \dot{x}_r(t;p) = A_r(p)x_r(t;p) + B_r u(t;p),$$
  
$$y_r(t;p) = C_r x_r(t;p),$$

where matrices  $V_r \in \mathbb{R}^{n \times r}$  and  $W_r \in \mathbb{R}^{n \times r}$  determine reduced system

$$E_r = (W_r)^T E V_r,$$
  $A_r = (W_r)^T A V_r,$   
 $B_r = (W_r)^T B$  and  $C_r = C V_r.$ 

For set of sampling parameters  $p^1,\ldots,p^s$  one can calculate truncation matrices and for global basis we can construct truncation matrices by  $V=[V^1_r,\ldots,V^s_r]$  and  $W=[W^1_r,\ldots,W^s_r]$ .

Problem: reduced order model depends on sampling parameters, but also which sampling one should use .

<sup>&</sup>lt;sup>1</sup>[Benner/Cohen/Ohlberger/Willcox2017], [Benner/Gugercin/Willcox2015], [Quarteroni/Manzoni/Negri2016], [Quarteroni/Rozza/Manzoni2011]



# We would like to remove the need for parametric sampling, which requires identifying particular parameters of interest!

We consider system where A(p) depends on  $k \ll n$  parameters  $p=(p_1,p_2,\ldots,p_k)$  such that we may write

$$A(p) = A_0 + U \operatorname{diag}(p_1, p_2, \dots, p_k)V^T = A_0 + \sum_{i=1}^k p_i u_i v_i$$

where  $U, V \in \mathbb{R}^{n \times k}$  are fixed. Full-order transfer function

$$\mathbf{H}(s;p) = C(sE - A(p))^{-1}B.$$

Aim: to produce a ROM that retains the structure of parametric dependence and offers uniformly high fidelity across the full parameter range.





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# Structure in damping example.

By defining the state-vector  $x = [q^T \ \dot{q}^T]^T$  we obtain:

$$\begin{bmatrix} I & 0 \\ 0 & M \end{bmatrix} \dot{x}(t) = A(p)x(t) + \begin{bmatrix} 0 \\ E_2 \end{bmatrix} w(t),$$
 
$$z(t) = \begin{bmatrix} H_1 & 0 \end{bmatrix} x(t), \text{ where}$$
 
$$A(p) = \begin{bmatrix} 0 & I \\ -K & -C_{int} \end{bmatrix} + \begin{bmatrix} 0 \\ B_2 \end{bmatrix} \operatorname{diag}(p_1, p_2, \dots, p_k) \begin{bmatrix} 0 & B_2^T \end{bmatrix}.$$

# Further extensions to the cases with higher rank.

E.g.  $A(p)=A_0+p_1A_1+p_2A_2$  where both  $A_1,A_2$  have rank-2.

Then, one can write  $A_1 = [u_1 \ u_2][v_1 \ v_2]^T$  and  $A_2 = [u_3 \ u_4][v_3 \ v_4]^T$ . With  $U = [u_1 \ u_2 \ u_3 \ u_4]$  and  $V = [v_1 \ v_2 \ v_3 \ v_4]$  we obtain

$$A(p) = A_0 + p_1 A_1 + p_2 A_2 = A_0 + U \operatorname{diag}(p_1, p_1, p_2, p_2) V^T.$$





#### The key observation!

$$\mathbf{H}(s;p) = C\left(\widehat{A}(s) - U \operatorname{diag}(p_1, p_2, \dots, p_k)V^T\right)^{-1} B, \ \widehat{A}(s) = sE - A_0.$$

We use the Sherman-Morrison-Woodbury formula.

$$\mathbf{H}(s;p) = \mathbf{H}_1(s) - \mathbf{H}_2(s)D(p)(I_k + D(p)\mathbf{H}_3(s)D(p))^{-1}D(p)\mathbf{H}_4(s),$$

where parameters are encoded in diagonal matrix

$$D(p) = \mathrm{diag}(\sqrt{p}_1, \sqrt{p}_2, \dots, \sqrt{p}_k)$$
 and

$$\mathbf{H}_1(s) = C\widehat{A}(s)^{-1}B,$$

$$\mathbf{H}_2(s) = C\widehat{A}(s)^{-1}U,$$

$$\mathbf{H}_3(s) = V^T \widehat{A}(s)^{-1} U,$$

$$\mathbf{H}_4(s) = V^T \widehat{A}(s)^{-1} B.$$

we construct a parameterized reduced order model by using four subsystems which **do not depend on parameters**:

$$[E, A_0, B, C], [E, A_0, U, V^T], [E, A_0, U, C], \text{ and } [E, A_0, B, V^T].$$





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# Approach 1: Reduced model based on vector fitting approach

#### Offline steps

• For the predetermined points in the complex plane  $\xi_1, \dots, \xi_N$  calculate

$$\mathbf{H}_1(\xi_i), \, \mathbf{H}_2(\xi_i), \, \mathbf{H}_3(\xi_i), \, \mathbf{H}_4(\xi_i) \quad \text{for} \quad i = 1, \dots, N.$$

These samples do not depend on parameters!

# Online steps

- For any given parameter  $p=(p_1,p_2,\ldots,p_k)$  calculate  $\mathbf{H}(\xi_i;p)$  for  $i=1,\ldots,N$  using obtained formula.
- Based on  $\mathbf{H}(\xi_1; p), \dots, \mathbf{H}(\xi_N; p)$  obtain reduced system with transfer function  $\widehat{\mathbf{H}}(s; p)$  using vector fitting approach.

The quality of approximations is determined by

$$e(\mathbf{H}(\cdot;p)), \widehat{\mathbf{H}}(\cdot;p))) = \sum_{i=1}^{N} \left\| \mathbf{H}(\xi_i;p) - \widehat{\mathbf{H}}(\xi_i;p) \right\|_F^2 / \sum_{i=1}^{N} \left\| \mathbf{H}(\xi_i;p) \right\|_F^2.$$





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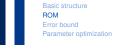
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# Approach 2: ROM based on reduction of subsystems

#### Offline steps

 For underlaying subsystems calculate reduced systems using model reduction techniques for non-parametric systems

$$\begin{split} & [E,A_0,B,C] \to \widehat{\mathbf{H}}_1(s), \text{ using order } r_1; \\ & [E,A_0,U,V^T] \to \widehat{\mathbf{H}}_2(s), \text{ using order } r_2; \\ & [E,A_0,U,C] \to \widehat{\mathbf{H}}_3(s), \text{ using order } r_3; \\ & [E,A_0,B,V^T] \to \widehat{\mathbf{H}}_4(s), \text{ using order } r_4; \end{split}$$

e.g. using balanced truncation or IRKA approach.

#### Online steps

• For any given parameter  $p=(p_1,p_2,\ldots,p_k)$  obtain approximated system  $\widehat{\mathbf{H}}(s;p)$  by

$$\mathbf{H}(s; \mathbf{p}) \approx \widehat{\mathbf{H}}_1(s) - \widehat{\mathbf{H}}_2(s)D(\mathbf{p})(I + D(\mathbf{p})\widehat{\mathbf{H}}_3(s)D(\mathbf{p}))^{-1}D(\mathbf{p})\widehat{\mathbf{H}}_4(s)$$





## Uniform stability of the parameterized reduced model

#### **Theorem**

Suppose that the full parameterized model  $\mathbf{H}(s,p)$  has been decomposed into subsystems  $\mathbf{H}_1(s)$ ,  $\mathbf{H}_2(s)$ , and  $\mathbf{H}_4(s)$  that are each asymptotically stable, and a subsystem  $\mathbf{H}_3(s)$  that is positive real. If the corresponding reduced subsystems  $\widehat{\mathbf{H}}_1(s)$ ,  $\widehat{\mathbf{H}}_2(s)$ , and  $\widehat{\mathbf{H}}_4(s)$  retain asymptotic stability, and  $\widehat{\mathbf{H}}_3(s)$  retains positive-realness, then the reduced parameterized model  $\widehat{\mathbf{H}}(s,p)$  in

$$\widehat{\mathbf{H}}(s; \mathbf{p}) = \widehat{\mathbf{H}}_1(s) - \widehat{\mathbf{H}}_2(s)D(\mathbf{p})(I + D(\mathbf{p})\widehat{\mathbf{H}}_3(s)D(\mathbf{p}))^{-1}D(\mathbf{p})\widehat{\mathbf{H}}_4(s).$$

is uniformly asymptotically stable for nonnegative parameters encoded in p.



In order to calculate error bound we consider full order transfer function

$$\mathbf{H}(s; \mathbf{p}) = \mathbf{H}_1(s) - \mathbf{H}_2(s)D(\mathbf{p})(I_k + D(\mathbf{p})\mathbf{H}_3(s)D(\mathbf{p}))^{-1}D(\mathbf{p})\mathbf{H}_4(s),$$

and corresponding reduced order transfer function

$$\widehat{\mathbf{H}}(s;p) = \widehat{\mathbf{H}}_1(s) - \widehat{\mathbf{H}}_2(s)D(p)(I_k + D(p)\widehat{\mathbf{H}}_3(s)D(p))^{-1}D(p)\widehat{\mathbf{H}}_4(s),$$

we would like to have upper bound for the error

$$\|\mathbf{H}(\cdot; \mathbf{p}) - \widehat{\mathbf{H}}(\cdot; \mathbf{p})\| \le ?$$



#### **Error bound**

It can be shown that

$$\mathbf{H}(\cdot;p) - \widehat{\mathbf{H}}(\cdot;p) = [\mathbf{H}_1 - \widehat{\mathbf{H}}_1] + [\widehat{\mathbf{H}}_2 - \mathbf{H}_2]D(p)(I + D(p)\widehat{\mathbf{H}}_3D(p))^{-1}D(p)\widehat{\mathbf{H}}_4 + \\ + \mathbf{H}_2D(p)(I + D(p)\widehat{\mathbf{H}}_3D(p))^{-1}D(p)[\widehat{\mathbf{H}}_4 - \mathbf{H}_4] + \\ + \mathbf{H}_2D(p)(I + D(p)\widehat{\mathbf{H}}_3D(p))^{-1}D(p)[\mathbf{H}_3 - \widehat{\mathbf{H}}_3]D(p)(I + D(p)\mathbf{H}_3D(p))^{-1}D(p)\widehat{\mathbf{H}}_4$$

Thus, we have

$$\begin{split} \|\mathbf{H}(\cdot;p) - \widehat{\mathbf{H}}(\cdot;p)\| &\leq \|\mathbf{H}_{1} - \widehat{\mathbf{H}}_{1}\| + \|\widehat{\mathbf{H}}_{2} - \mathbf{H}_{2}\| \|D(p) (I + D(p)\widehat{\mathbf{H}}_{3}D(p))^{-1}D(p)\widehat{\mathbf{H}}_{4}\| + \\ &+ \|\mathbf{H}_{2}D(p) (I + D(p)\mathbf{H}_{3}D(p))^{-1}D(p)[\widehat{\mathbf{H}}_{4} - \mathbf{H}_{4}]\| + \\ &+ \|\mathbf{H}_{2}D(p) (I + D(p)\widehat{\mathbf{H}}_{3}D(p))^{-1}D(p)\| \|\mathbf{H}_{3} - \widehat{\mathbf{H}}_{3}\| \|D(p) (I + D(p)\mathbf{H}_{3}D(p))^{-1}D(p)\widehat{\mathbf{H}}_{4}\| \end{split}$$





#### **Error bound**

It can be shown that

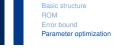
$$\mathbf{H}(\cdot;p) - \widehat{\mathbf{H}}(\cdot;p) = [\mathbf{H}_1 - \widehat{\mathbf{H}}_1] + [\widehat{\mathbf{H}}_2 - \mathbf{H}_2]D(p)(I + D(p)\widehat{\mathbf{H}}_3D(p))^{-1}D(p)\widehat{\mathbf{H}}_4 + \\
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Thus, we have

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Which means that we have a bound in terms of

$$\|\mathbf{H}(\cdot; p) - \widehat{\mathbf{H}}(\cdot; p)\| \lesssim \underbrace{\varepsilon_1 + \varepsilon_2 f_1(p, \widehat{\mathbf{H}}_3, \widehat{\mathbf{H}}_4) + \varepsilon_4 f_2(p, \widehat{\mathbf{H}}_2, \widehat{\mathbf{H}}_3) + \varepsilon_3 f_3(p, \widehat{\mathbf{H}}_2, \widehat{\mathbf{H}}_3, \widehat{\mathbf{H}}_4)}_{f_1(p)}$$





# Surrogate optimization with reduced parametric models

A major cost in parameter optimization is the repeated evaluation of the  $\mathcal{H}_2$  norm.

We can use the approach 1 or 2 to accelerate computational cost, so we solve a surrogate optimization problem

$$\hat{p}^* = \arg\min_{p \in \Omega} \|\widehat{\mathbf{H}}(\cdot, p)\|_{\mathcal{H}_2},$$

where the reduced parametric transfer function  $\hat{\mathbf{H}}(\cdot,p)$  will be constructed using either approach 1 or approach 2, without need for parameter sampling.

Assume  $p^*$  is the minimizer and note that

$$\|\mathbf{H}(\cdot, p^{\star})\|_{\mathcal{H}_{2}} \leq \|\mathbf{H}(\cdot, p^{\star}) - \widehat{\mathbf{H}}(\cdot, p^{\star})\|_{\mathcal{H}_{2}} + \|\widehat{\mathbf{H}}(\cdot, p^{\star})\|_{\mathcal{H}_{2}}.$$

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The surrogate optimization problem will minimize the second term.





# Parameter optimization using reduced models via approach 1

- 1: Choose the reduced order so that  $e(p^0) < \tau$ .
- 2: Solve the surrogate optimization problem

$$\hat{p}^{\star} = \arg\min_{p} \left\| \widehat{\mathbf{H}}(\cdot, p) \right\|_{\mathcal{H}_2}$$

with the initial guess  $p^0$  and VF approach for  $\widehat{\mathbf{H}}_p$ , using  $\{\mathbf{H}_i(\xi_i)\}_{i=1}^N$ .

- 3: **while** minimizer  $p^{\star}$  such that  $e(p^{\star}) > \tau$  **do**
- 4:  $p^0 = \hat{p}^*$
- 5: Increase the reduced order so that  $e(\hat{p}^{\star}) < \tau$ .
- 6: Determine the new minimizer by solving the

$$\hat{p}^{\star} = \arg\min_{p} \left\| \widehat{\mathbf{H}}(\cdot, p) \right\|_{\mathcal{H}_2}$$

using the updated  $\widehat{\mathbf{H}}$ , the initial guess  $p^0$ , and tolerance  $\nu$ .

#### 7: end while



# Parameter optimization using reduced models via approach 2

- 1: Choose the reduced orders  $r_1, r_2, r_3, r_4$  (and  $\widehat{\mathbf{H}}_1, \widehat{\mathbf{H}}_2, \widehat{\mathbf{H}}_3, \widehat{\mathbf{H}}_4$ ) so that  $f(p^0) < \tau \, \|\widehat{\mathbf{H}}(\cdot, p^0)\|_{\mathcal{H}_2}$ .
- 2: Solve the surrogate optimization problem

$$\hat{p}^{\star} = \arg\min_{p} \left\| \widehat{\mathbf{H}}(\cdot, p) \right\|_{\mathcal{H}_2}$$

with the initial guess  $p^0$  and tolerance  $\nu$ .

- 3: while minimizer  $p^\star$  such that  $f(p^\star) > \tau \, \| \hat{\mathbf{H}}(\cdot, p^0) \|_{\mathcal{H}_2}$  do
- 4:  $p^0 = \hat{p}^*$
- 5: Increase the orders  $r_1, r_2, r_3, r_4$  s.t.  $f(\hat{p}^{\star}) < \tau \, \| \widehat{\mathbf{H}}(\cdot, p^0) \|_{\mathcal{H}_2}$ .
- 6: Determine the new minimizer by solving the

$$\hat{p}^{\star} = \arg\min_{p} \left\| \widehat{\mathbf{H}}(\cdot, p) \right\|_{\mathcal{H}_{2}}$$

using the updated  $\hat{\mathbf{H}}$ , the initial guess  $p^0$ , and tolerance  $\nu$ .

7: end while



We consider example from [Penzl 1999]. The full-order system is known and defined by state-space matrices

$$A = \operatorname{diag}(A_1(p_1), A_2(p_2), A_3(p_3), -1, -2, \dots, -N)$$

$$A_i(p_i) = \begin{bmatrix} -1 & p_i \\ -p_i & -1 \end{bmatrix}, \quad \text{for} \quad i = 1, \dots, 3$$

Matrix  $C \in \mathbb{R}^{1 \times (N+6)}$  where

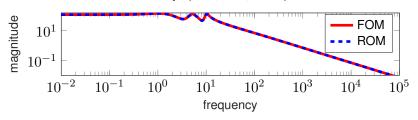
$$c_i = \begin{cases} 10, & i = 1, \dots, 6, \\ 1, & i = 7, \dots, N. \end{cases}$$

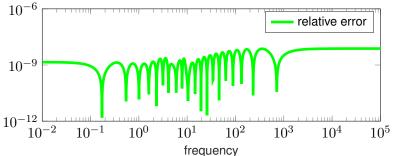
 $B=C^T$  and number of states N=100. The parameters  $p_1,p_2,p_3$  represent the imaginary part of the two eigenvalues of the diagonal block  $A_i(p_i)$ , respectively. Here we use that  $p_2=5p_1$  and  $p_3=20p_1$ . We illustrate approach based on balanced truncation of subsystems where four underlaying subsystems were reduced to dimensions 10, 1, 6, 1.





#### p=(1.00, 5.00, 20.00)





Introduction
Parametric model reduction
Numerical experiments

Penzl example Thermal Model Damping example





We consider thermal conduction in a semiconductor chip from Oberwolfach Benchmark Collection.

The full-order system is:

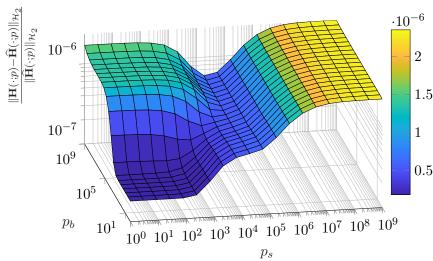
$$\begin{split} E\dot{x} &= (A - p_t A_t - p_b A_b - p_s A_s)x + Bu\\ y &= Cx, \quad \text{where} \end{split}$$

- $E \in \mathbb{R}^{4257 \times 4257}$  corresponds to heat capacity and A to heat conductivity matrix
- $B \in \mathbb{R}^{1 \times 4257}$  is the load vector and  $C \in \mathbb{R}^{7 \times 4257}$
- A<sub>t</sub>, A<sub>b</sub> and A<sub>s</sub> are the diagonal matrices from the discretization of the convection boundary conditions with ranks 111, 99 and 31, resp.
- Parameters  $p_t, p_b, p_s$  represent film coefficients.

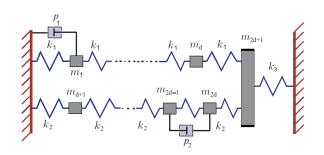




We fix  $p_t=1000$  and vary both  $p_b$  and  $p_s$  between 1 and  $10^9$ . Reduced dim. of subsystems:  $r_1=46, r_2=66, r_3=200, r_4=16$ .







#### The mass and the stiffness matrix are given by

$$K = \begin{bmatrix} K_{11} & -\kappa_1 \\ K_{22} & -\kappa_2 \\ -\kappa_1^T & -\kappa_2^T & k_1 + k_2 + k_3 \end{bmatrix}, K_{ii} = k_i \begin{bmatrix} 2 & -1 \\ -1 & 2 & -1 \\ & \ddots & \ddots & \ddots \\ & & -1 & 2 & -1 \\ & & & & -1 & 2 \end{bmatrix},$$

$$\kappa_i = \begin{bmatrix} 0 & \dots & 0 & k_i \end{bmatrix}$$
 for  $i = 1, 2$  and  $M = \operatorname{diag}(m_1, m_2, \dots, m_n)$ .



$$d = 900 \Rightarrow n = 1801$$
, with  $m_{1801} = 1000$  and

$$m_i = \begin{cases} 1000 - \frac{i}{2}, & i = 1, \dots, 450, \\ i + 325, & i = 451, \dots, 900, \\ 1300 - \frac{i}{4}, & i = 901, \dots, n. \end{cases}$$

The stiffness values are given by

$$k_1 = 500, k_2 = 200, k_3 = 300.$$

The primary excitation are 5 disturbances applied to the 4 masses closest to the left-hand side and one mass closest to the right-hand side of oscillator.

We are interested in 2 displacements, i. e.

$$z(t;p) = [q_{400}(t;p) \quad q_{1300}(t;p)]^T.$$





Internal damping is a small multiple of critical damping

$$C_{int} = 0.04 \cdot M^{1/2} \left( M^{-1/2} K M^{-1/2} \right)^{1/2} M^{1/2}.$$

We consider four dampers with gains  $p_1, p_2, p_3$  and  $p_4$  where geometry of positions is given by

$$B_2 = [e_{j_1} - e_{j_1+10}, e_{j_2}, e_{j_3}, e_{j_3} - e_{j_3+100}],$$

with  $j_1 \in \{100, 300, 500, 700\}$ ,  $j_2 \in \{150, 350, 550, 750\}$ ,  $j_3 \in \{1400, 1700\} \Rightarrow$  32 different damping configurations at which  $\|\cdot\|_{\mathcal{H}_2}$  norm was minimized.

Gains were optimized with starting point  $p^0 = (100, 100, 100, 100)$  using the full-order model and using proposed reduced systems.



#### In the approach based on balanced truncation of subsystems:

 in all damping configurations, starting reduced dimensions of four subsystems were 280, 300, 480, 430, resp.

# In the approach based on vector fitting approach

- initial points  $\xi_i$ ,  $i=1,\ldots,N$ , for N=500 depending on modally damped system.
- 130 initial poles (chosen using from dominant poles).

The stoping tolerance for parameter optimization was 0.005.

#### Time ratio

In average case for one optimization of parameters, new approach was faster:

- pprox 7.8 times, with usage of reduced model based on balanced truncation of subsystems,
- $\approx 60$  times, with usage of reduced model based on vector fitting approach.



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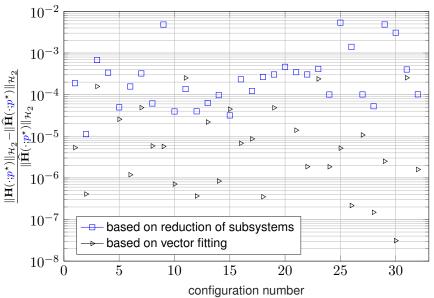
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#### Conclusion:

- We have introduced a framework for producing reduced order models of dynamical systems having an affine, low-rank parametric structure.
  - Approach 1: Reduced model based on vector fitting approach.
  - Approach 2: ROM based on reduction of subsystems.
- The new framework does not require any sampling in the parameter domain and instead parametrically combines intermediate subsystems that are nonparametric.
- Can guarantee uniform stability of the aggregated reduced model across the entire parameter domain in many cases.
- These approaches can be deployed efficiently in parameter optimization problems as well.



Thank you for your attention!