

Interpolation-based parametric model reduction for efficient damping optimization



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We consider vibrational system

$$M\ddot{q}(t) + \overbrace{(C_{int} + B_2GB_2^T)}^{C=\text{damping part}}\dot{q}(t) + Kq(t) = E_2w(t),$$
$$z(t) = H_1q(t).$$

- $M, K > 0$ mass and stiffness,
- E_2 primary excitation matrix,
- C_{int} internal damping e.g. $C_{int} = \alpha_c C_{crit}$, where $C_{crit} = 2M^{1/2}\sqrt{M^{-1/2}KM^{-1/2}}M^{1/2}$,
- $G = \text{diag}(g_1, g_2, \dots, g_p)$, $g_i \geq 0$ represents coefficients of damper,
- q state vector and z is output vector determined by H_1 ,
- vector w corresponds to primary excitation input.



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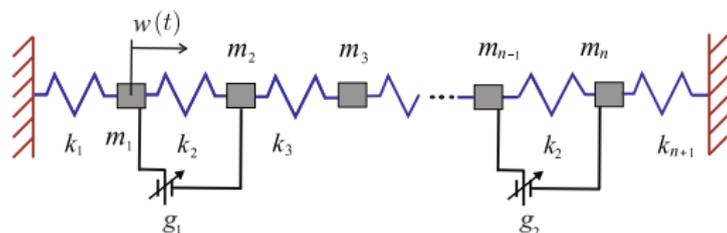
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Example: n -mass oscillator or oscillator ladder



$$M = \text{diag}(m_1, m_2, \dots, m_n), \quad C = B_2 G B_2^T + \alpha_c C_{crit},$$

$$B_2 G B_2^T = g_1 (e_k - e_{k+1})(e_k - e_{k+1})^T + g_2 (e_j - e_{j+1})(e_j - e_{j+1})^T.$$

$$K = \begin{pmatrix} k_1 + k_2 & -k_2 & & & & \\ -k_2 & k_2 + k_3 & -k_3 & & & \\ & & \ddots & \ddots & \ddots & \\ & & & -k_{n-1} & k_{n-1} + k_n & -k_n \\ & & & & -k_n & k_n + k_{n+1} \end{pmatrix}.$$



Linearization

- Using Φ which simultaneously diagonalizes M and K

$$\Phi^T K \Phi = \Omega^2 = \text{diag}(\omega_1^2, \dots, \omega_n^2) \quad \text{and} \quad \Phi^T M \Phi = I,$$

$$0 < \omega_1 \leq \omega_2 \leq \dots \leq \omega_n.$$

- with $\hat{x}_1 = \Omega \Phi^{-1} q(t)$ and $\hat{x}_2 = \Phi^{-1} \dot{q}(t)$ system can be written as :

$$\dot{\hat{x}}(t) = \hat{A} \hat{x}(t) + \begin{bmatrix} 0 \\ \Phi^T E_2 \end{bmatrix} w(t),$$

$$z(t) = \begin{bmatrix} H_1 \Phi \Omega^{-1} & 0 \end{bmatrix} x(t), \quad \text{where}$$

$$\hat{x} = \begin{bmatrix} \hat{x}_1 \\ \hat{x}_2 \end{bmatrix}, \quad \hat{A} = \begin{bmatrix} 0 & \Omega \\ -\Omega & -\alpha \Omega - \Phi^T B_2 G B_2^T \Phi \end{bmatrix}.$$



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Problem :

Determine "optimal" damping matrix C which will minimize the effect of the input w on the output z .

For criterion one can use e.g.:

- \mathcal{H}_2 norm of a system

$$\|H\|_{\mathcal{H}_2} = \left(\frac{1}{2\pi} \int_{-\infty}^{+\infty} \text{tr} (H(j\omega)^* H(j\omega)) d\omega \right)^{\frac{1}{2}}$$

transfer function $H(s) = H_1(s^2 M + sC + K)^{-1} E_2$, $s \in \mathbb{C}$.

- \mathcal{H}_∞ norm of a system

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Optimization problem for \mathcal{H}_2 norm

Impulse response energy leads to

$$\hat{A}^T \hat{X} + \hat{X} \hat{A} = -\hat{H}^T \hat{H},$$

$$\hat{A} = \begin{bmatrix} 0 & \Omega \\ -\Omega & -\alpha\Omega - \Phi^T B_2 G B_2^T \Phi \end{bmatrix}, \quad \hat{H} = \begin{bmatrix} H_1 \Phi \Omega^{-1} & 0 \end{bmatrix},$$

With $\hat{X} = \begin{bmatrix} X_{11} & X_{12} \\ X_{21} & X_{22} \end{bmatrix}$, it holds

$$J_2 = \text{tr} (E_2^T \Phi X_{22} \Phi^T E_2) \rightarrow \min .$$

Model order reduction: provides efficient approximation of energy J_2 needed for optimization of G .



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Model order reduction

With $W_r \in \mathbb{R}^{n \times r}$, $q(t) = W_r q_r(t)$ and $V_r \in \mathbb{R}^{n \times r}$ we obtain reduced system

$$\begin{aligned} M_r \ddot{q}_r(t) + C_r \dot{q}_r(t) + K_r q_r(t) &= E_r w(t) \quad \text{where} \\ M_r &= W_r^* M V_r, C_r = W_r^* C V_r, \\ K_r &= W_r^* K V_r, E_r = W_r^* E_2, H_r = H_1 V_r \end{aligned}$$

Transfer function of reduced system is

$$H_r(s) = H_r (s^2 M_r + s C_r + K_r)^{-1} E_r, \quad s \in \mathbb{C}.$$

We choose W_r and V_r to enforce (tangential) interpolation.



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Model reduction by Interpolation

For selected points $\sigma_1, \sigma_2, \dots, \sigma_r \in \mathbb{C}$ and directions b_1, \dots, b_r and c_1, \dots, c_r find $H_r(s)$ such that

$$\begin{aligned}c_i^T H(\sigma_i) &= c_i^T H_r(\sigma_i) \\ H(\sigma_i) b_i &= H_r(\sigma_i) b_i \\ c_i^T H'(\sigma_i) b_i &= c_i^T H_r'(\sigma_i) b_i.\end{aligned}$$

Moreover: we would like to have an approximation s.t. $\|\cdot\|_{\mathcal{H}_2}$ is optimally approximated, i.e. find local minimizer for $\|H - H_r\|_{\mathcal{H}_2}$.

This can be done in general framework efficiently¹ using structure preserving Model Reduction.

Additionally to preserve structure in second order system: $V_r = W_r$.

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Alg. 1: Iterative rational Krylov algorithm (IRKA)

Require: System matrices defining, and given gains g_1, g_2, \dots, g_p ,

initial shift selection $\sigma_1 \dots, \sigma_r$; initial tangent directions r_1, \dots, r_r .

$$1: V_r = [(\sigma_1^2 M + \sigma_1 C + K)^{-1} B r_1, \dots, (\sigma_r^2 M + \sigma_r C + K)^{-1} B r_r];$$

2: **for** $j = 1, \dots, \max_{it}$ **do**

3: Form reduced system determined by: $M_r = V_r^* M V_r$,

$$C_r = V_r^* C V_r, K_r = V_r^* K V_r, E_r = V_r^* E_2, H_r = H_1 V_r$$

4: Consider quadratic eigenvalue problem

$(M_r \lambda_i^2 + C_r \lambda_i + K_r) x_i = 0, x_i \neq 0, i = 1, \dots, 2r$ and reduce system to r states in order to have r eigenvalues $\tilde{\lambda}_1, \dots, \tilde{\lambda}_r$ closed under conjugation

5: $\sigma_i = -\tilde{\lambda}_i$ and update $r_i, i = 1, \dots, r$

$$6: V_r = [(\sigma_1^2 M + \sigma_1 C + K)^{-1} B r_1, \dots, (\sigma_r^2 M + \sigma_r C + K)^{-1} B r_r];$$

7: **if** converged **then**

8: **return** $V = V_r$

9: **end if**

10: **end for**



Usage of modal coordinates

For given shift σ and direction r_i in solving

$$(\sigma^2 M + \sigma_1 C + K)^{-1} B r_i$$

we apply reduction directly to system in modal coordinates.

Here we use Sherman-Morrison-Woodbury formula:

$$\begin{aligned} (\sigma^2 I + \sigma \alpha \Omega + \sigma \Phi^T B_2 G B_2^T \Phi + \Omega^2)^{-1} \Phi^T B r_i &= T^{-1} \Phi^T B r_i \\ &\quad - s T^{-1} B_g (I_p + s B_g^T T^{-1} B_g)^{-1} B_g^T T^{-1} \Phi^T B r_i \end{aligned}$$

where

$$\begin{aligned} T &= (\sigma^2 I + \sigma \alpha \Omega + \Omega^2), \\ B_g &= \Phi^T B_2 \text{diag}(\sqrt{g_1}, \dots, \sqrt{g_p}), \end{aligned}$$

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Internal reduction

- a) internal reduction based on balanced truncation;
used balanced truncation method applied to the linearized model.
- b) internal reduction based on IRKA algorithm;
apply additional reduction using IRKA approach to linearized model.
- c) internal reduction based on dominant poles;
Since the transfer function

$$F(s) = \sum_{i=1}^{2n} \frac{R_i}{s - \lambda_i} \quad \text{with} \quad R_i = (H_1 x_i)(y_i^* E_2) \lambda_i,$$

where $\lambda_i \in \mathbb{C}$, x_i , y_i are, respectively, eigenvalues, right and left eigenvectors of the QEP.

We maintain the r poles with the largest values of $\frac{\|R_i\|}{|\operatorname{Re}(\lambda_i)|}$



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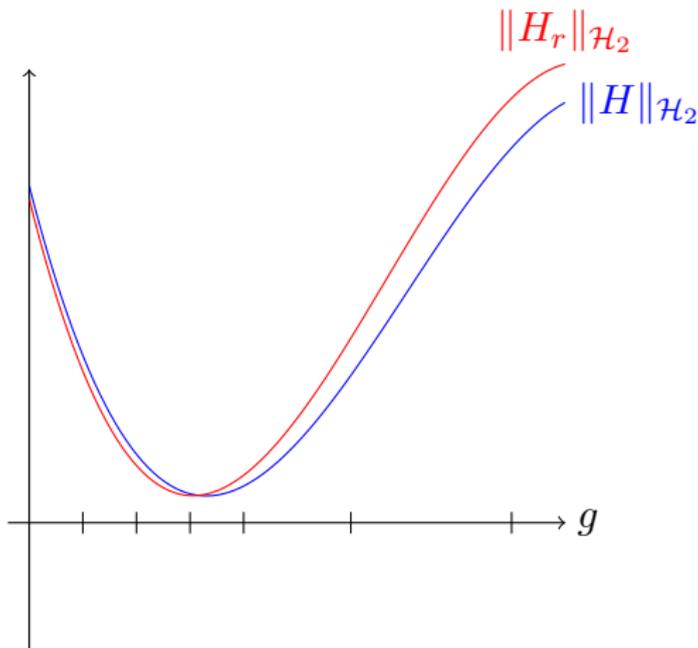
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We propose the following sampling strategies

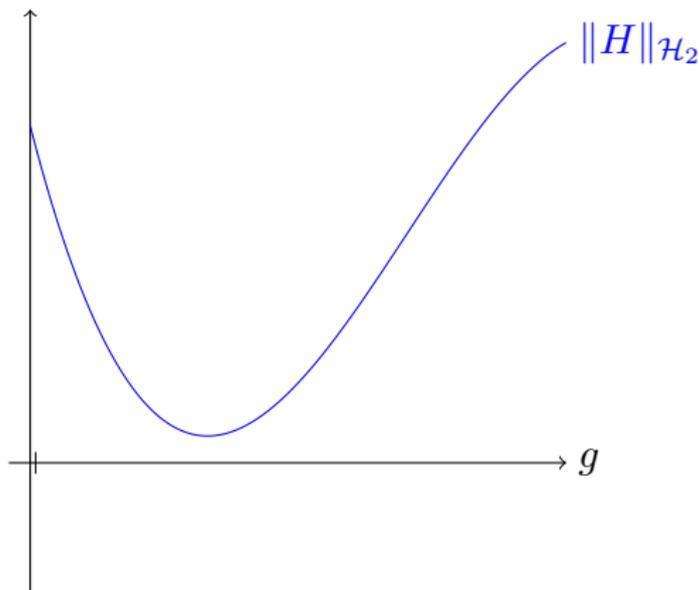
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- adaptive sampling during optimization.





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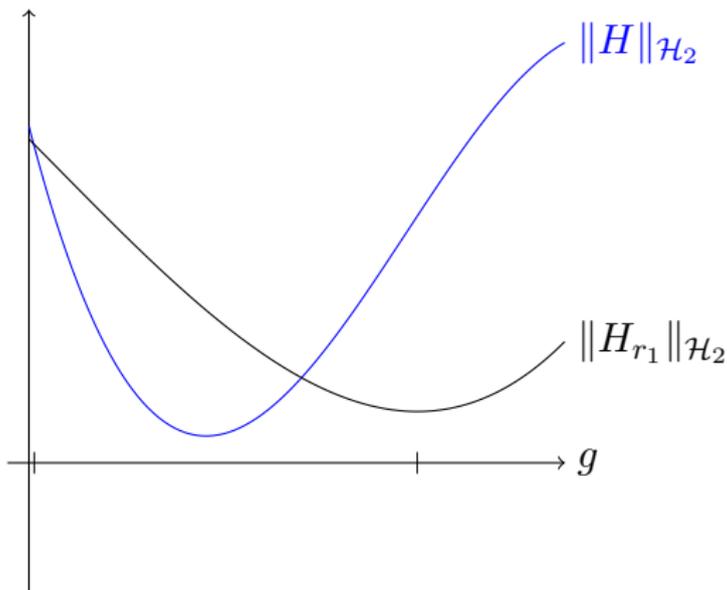
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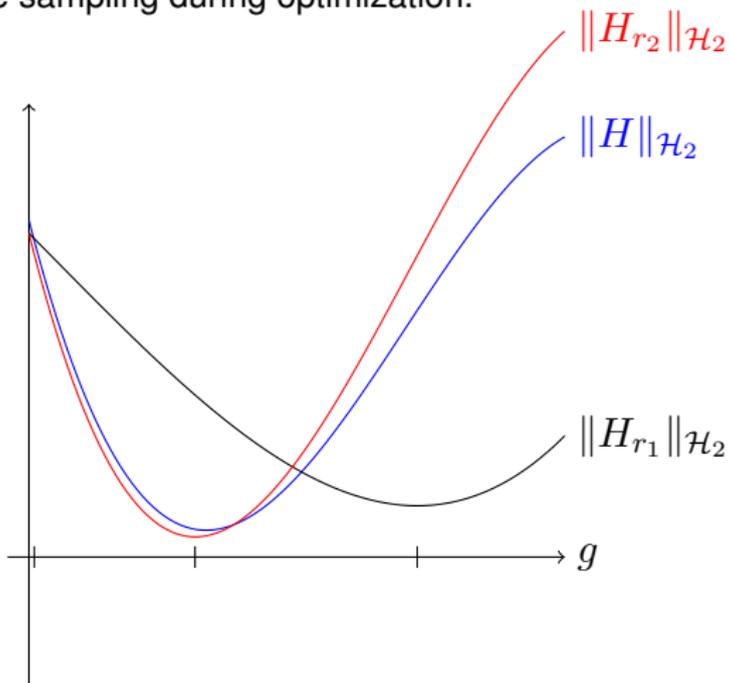
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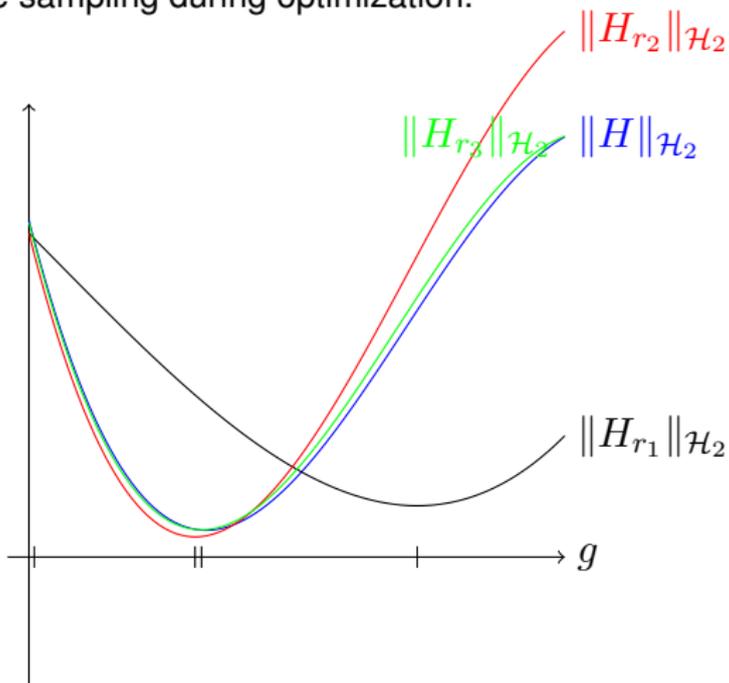
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Optimization approach using fixed sampling parameters

Algorithm 2:

Require: System matrices; initial value for shift selection $\sigma_1 \dots, \sigma_r$ and initial directions r_1, \dots, r_r ;
number of wanted poles k_{wanted} for each setting of parameters.;
set of sampling parameters g^1, \dots, g^m .

Ensure: Approximate optimal gains.

- 1: **for** $j = 1, \dots, m$ **do**
- 2: With IRKA Algorithm using gain g^i calculate V^i
- 3: **end for**
- 4: $X = \text{orth}([V^1, \dots, V^m])$.
- 5: Form a reduced system using X .
- 6: Find an optimal gains by using an appropriate optimization procedure on obtained reduced system.



Optimization approach using adaptive sampling

Algorithm 3:

Require: System matrices; initial value for shift selection $\sigma_1 \dots, \sigma_r$ and initial directions r_1, \dots, r_r ;
number of wanted poles k_{wanted} for each setting of parameters.;
the first sampling parameters g^0 .

Ensure: Approximate optimal gains.

- 1: $j = 0$;
- 2: **repeat**
- 3: With IRKA Algorithm using gain g^j calculate V^j
- 4: Form reduced system using $X = \text{orth}([V^0, V^1, \dots, V^j])$.
- 5: $j = j + 1$
- 6: Find an approximation of optimal gains by using obtained reduced system and denote it by g^j .
- 7: **until** $|g^j - g^{j-1}| < tol_g$
- 8: return g^j



Parametric dominant pole algorithm

Reduced system is obtained with $q(t) = Xq_k(t)$ where $X \in \mathbb{C}^{n \times k}$ span the eigenspaces associated with the k dominant poles, efficiently calculated.

For initial parameters $g^{(1)} = 0, g^{(2)}, \dots, g^{(m)}$ we merge together corresponding right eigenspaces $X^{(j)}$. \rightsquigarrow for initial parameters the original and reduced model have similar behavior near dominant poles.

Determination of sampling parameters $g^{(2)}, \dots, g^{(m)}$: adaptively, depending on residual error bound.

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Primary excitation matrix is applied to 10 consecutive masses, i.e.

$$E_2(471 : 481, 1 : 10) = \text{diag}(10, 20, 30, 40, 50, 50, 40, 30, 20, 10),$$

We are interested in the 18 states equally distributed

$$H_1(1 : 18, 100 : 100 : 1800) = I_{18 \times 18}$$

The geometry of external damping is determined by four dampers with

$$B_2 = [e_i \ e_{i+1} \ e_k \ e_{k+1}],$$

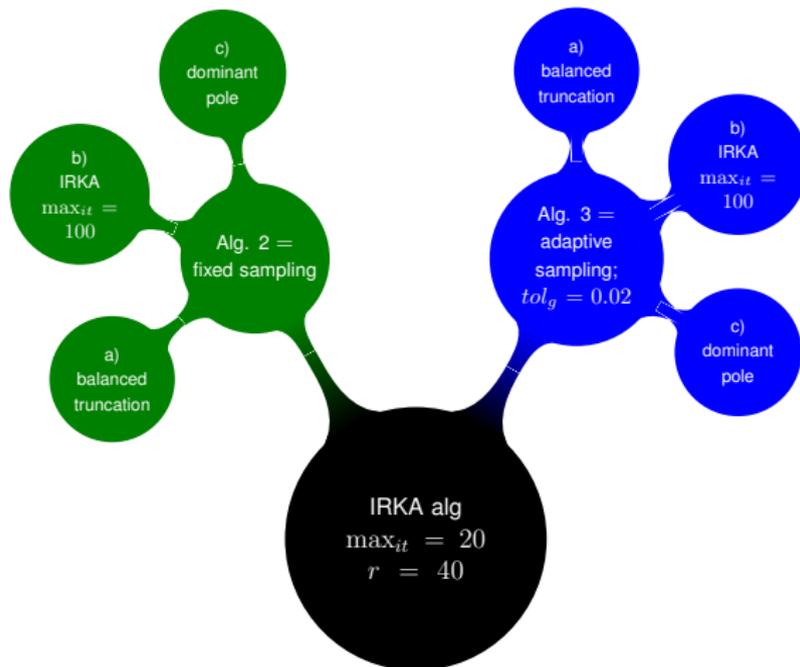
for 44 different damping configurations (i, k) , where

$$G = \text{diag}(g_1, g_1, g_2, g_2).$$



Comparison:

- IRKA with fixed sampling \leftrightarrow parametric dominant pole algorithm,
- IRKA with fixed sampling \leftrightarrow IRKA with adaptive sampling.





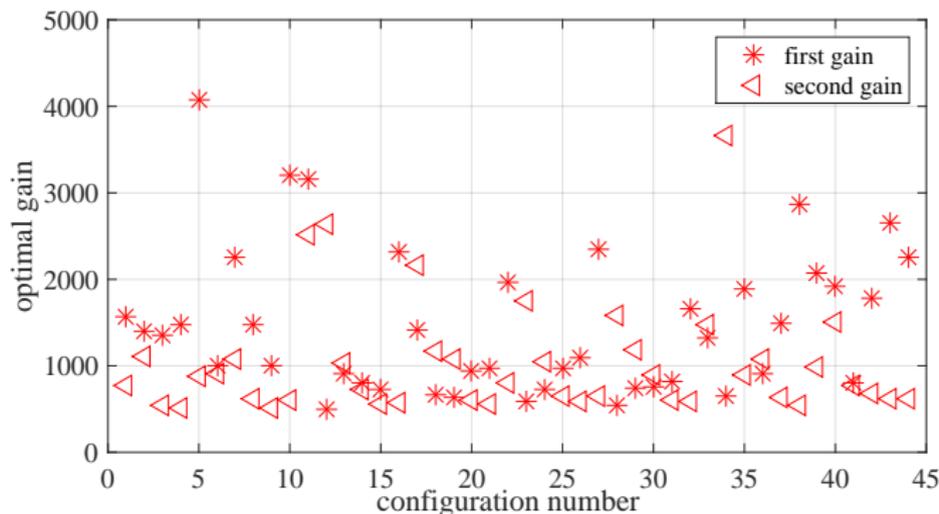
Gains for fixed sampling

$$g^{(0)} = (0, 0) \Rightarrow g^{(1)}$$

$$g^{(2)} = (1000, 1000)$$

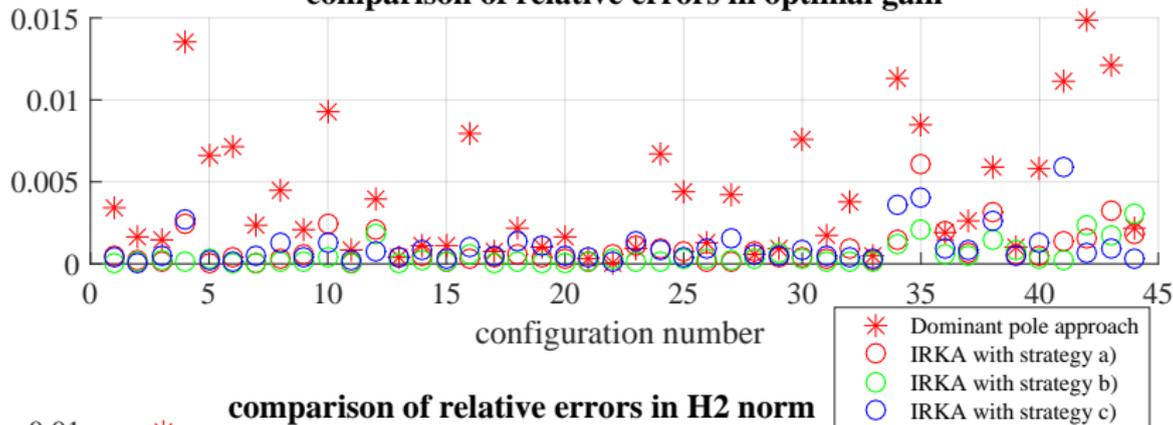
$$g^{(3)} = (100, 1000)$$

$$g^{(4)} = (1000, 100)$$

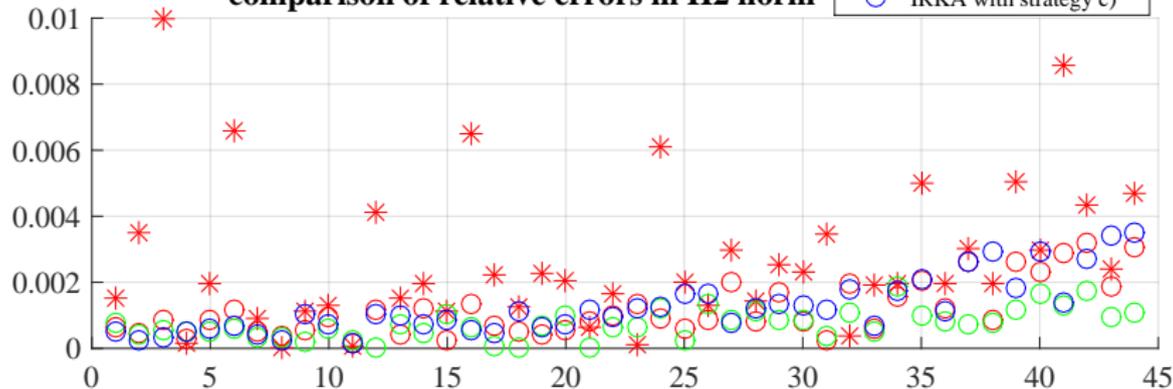




comparison of relative errors in optimal gain

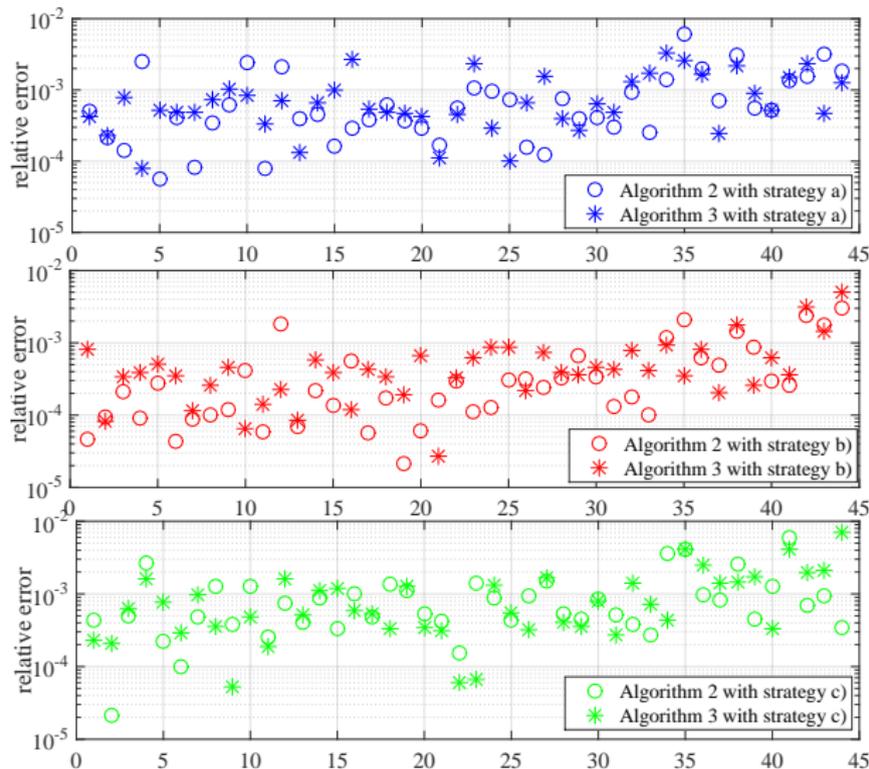


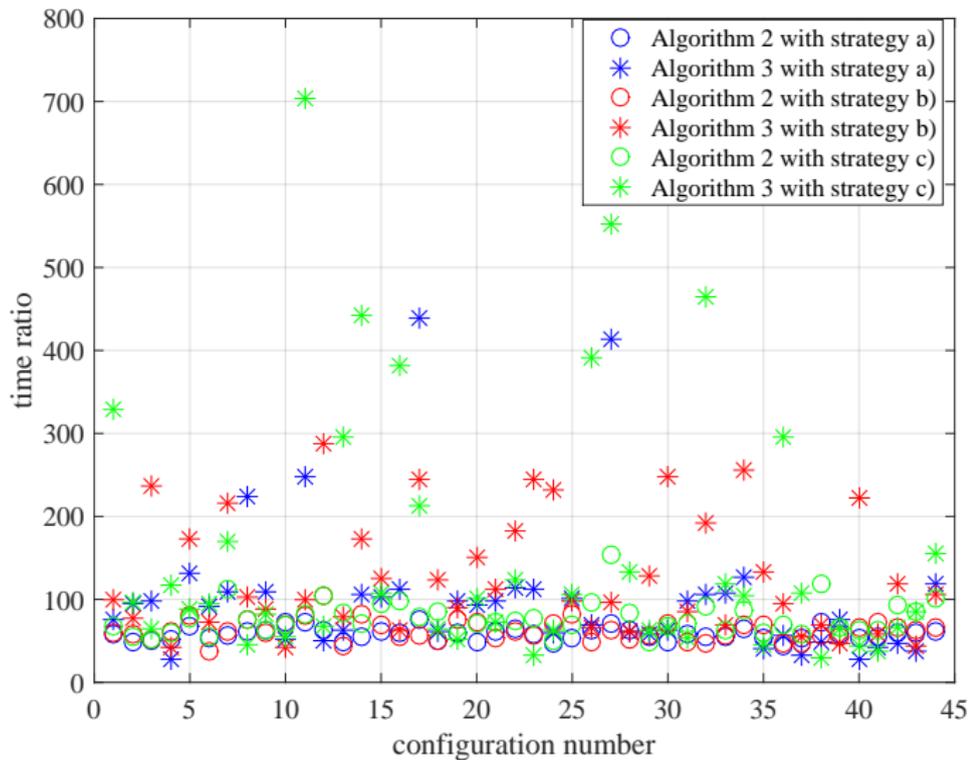
comparison of relative errors in H2 norm





Comparison of relative errors in optimal gain







Thank you for your attention!